## The solid solution structure of $BiSr_xCa_{1-x}O_{2.50}$

GUOHONG XIONG, MINQUAN WANG, XIANPING FAN Department of Materials Science and Engineering, Zhejiang University, Hangzhou 310027, People's Republic of China

GUANGLIE LU

The Center Laboratory, Hangzhou University, Hangzhou 310028, People's Republic of China

The formation and solid-solution structure of  $\text{BiSr}_x\text{Ca}_{1-x}\text{O}_{2.50}$  were studied by X-ray powder diffraction analysis, and the crystallography data of the phase are given. The crystal structure of  $\text{BiSr}_x\text{Ca}_{1-x}\text{O}_{2.50}$  belongs to the monoclinic system with space group P1*m*1 or P12/*m*1, and the cell parameters for BiCaO<sub>2.50</sub> (*x*=0.00) are *a*=1.8363 nm, *b*=0.5366 nm, *c*= 1.4670 nm and  $\beta$ =100.26°. BiSr<sub>x</sub>Ca<sub>1-x</sub>O<sub>2.50</sub> is a solid solution of Bi–Ca–O and Bi–Sr–O. When the strontium solid solubility Sr/Sr+Ca=0.50, the strontium dissolved in the phase reaches saturation, while the strontium solid solubility limit of the phase is between 0.67 and 0.75, and beyond this limit the crystal structure is greatly distorted.

### 1. Introduction

Bismuth-based superconductors in the series  $Bi_2Sr_2Ca_{n-1}Cu_nO_{\delta}$  [1, 2] are members of the structural family that includes thallium-containing compositions with the highest values of  $T_c$  yet reported. Unlike the thallium-system, the nominal three-layer bismuth analogue, Bi<sub>2</sub>Sr<sub>2</sub>Ca<sub>2</sub>Cu<sub>3</sub>O<sub>8</sub> (2223) is still difficult to synthesize in its pure form, for the formation of 2223 is a much slower process taking place in a very limited temperature range [3, 4]. It is therefore desirable to discover more about the reaction process in the BSCCO system with the goal of understanding the formation reaction of its superconducting phases. Once the reaction path has been found it can be modified by avoiding or promoting certain phases using binary or trinary oxide components as starting materials. Thus, the stability range of desired superconducting phases can be enlarged or their formation accelerated.

Previously, we studied systematically [5] the reaction process of the BSCCO system and found out that  $Bi_2Sr_2CaCu_2O_{\delta}$  (2212) is formed by the reaction of a Bi-Sr-Ca-O ternary unknown intermediate phase, together with CuO, SrO and CaO. This intermediate phase is a solid solution of Bi-Ca-O and Bi-Sr-O, and called interphase for short. From the results, we presented a new two-step method to prepare the 2212 phase through the presynthesized interphase. Using this method, it is easy to adjust the strontium solid solubility of 2212, which affects its electromagnetic properties greatly [5, 6]. Thus, it is necessary to study the solid solubility of the interphase. In the present paper, the formation, composition, and solid solution structure of the interphase is reported and the crystallography data of the phase are given.

### 2. Experimental procedure

Samples were prepared by (1) weighing and mixing analytically pure  $Bi_2O_3$ ,  $SrCO_3$  and  $CaCO_3$  in the desired proportions as shown in Table I, (2) grinding in an agate ball mill for 3 h, and (3) pressing the mixed powders into pellets. The pellets were sintered under the conditions listed in Table I. Sintering temperatures were selected according to the differential thermal analysis (DTA) curves of the mixed powders.

The diffraction data were collected using a D/max-III B type diffractometer using  $CuK_{\alpha}$  radiation at 40 kV and 20 mA. The scanning speed is 1° 2 $\theta$  min<sup>-1</sup>. The resulting 2 $\theta$  is rectified at 5°-25° and 25°-55° using tetradecanol-[1] (CH<sub>3</sub>(CH<sub>2</sub>)<sub>12</sub>CH<sub>2</sub>OH) and silicon as standard materials, respectively. Unit-cell parameters were calculated by using the program TREOR [7] and refined by least squares analysis. The cell parameters should be regarded as preliminary. Either single-crystal X-ray or electron diffraction studies will be required to refine the structure of this compound. Morphology was observed and microarea composition was analysed using a Hitachi S-570 scanning electron microscope (SEM) with energy-dispersive Xray spectroscopy (EDXS).

### 3. Results and discussion

# 3.1. The formation and the composition of the interphase

Fig. 1 shows the XRD spectra of Bi–Ca–O and Bi–Sr–Ca–O binary and ternary samples. Except for the diffraction peaks of formed  $Ca_7Bi_{10}O_{22}$  [8, 9], unreacted remaining SrCO<sub>3</sub> and a small amount of free CaO, the rest correspond well with each other, but they cannot conform to the already known diffraction

| ΤA | BLI | ΕI | Sample co | mpositions | and sin | tering   | conditions |
|----|-----|----|-----------|------------|---------|----------|------------|
|    |     | _  |           |            |         | <i>u</i> |            |

| Composition   | x, y                                 | Sintering conditions                                |  |  |  |  |
|---|--------------------------------------|---|--|--|--|--|
| BiSr. CaO <sub>2 50+</sub>                            | 0.00, 0.25, 1.00                     | 730 °C/5 h; 815 °C/5 h, quenched in liquid nitrogen |  |  |  |  |
| $BiCa_vO_{1-50+v}$                                    | 0.50, 0.75, 1.00                     | 800 °C/15 h, quenched in air                        |  |  |  |  |
| y 1.50 y  | 1.25, 1.50, 1.75                     |   |  |  |  |  |
| $\mathrm{BiSr}_{x}\mathrm{Ca}_{1-x}\mathrm{O}_{2.50}$ | 0.00, 0.25, 0.33<br>0.50, 0.67, 0.75 | 800-830 °C/24 h, quenched in air                    |  |  |  |  |



Figure 1 XRD patterns of the BiSr<sub>y</sub>CaO<sub>2.50+y</sub> (y = 0.00, 0.25, 1.00) samples sintered at 730 °C or 815 °C for 5 h. ( $\bullet$ ) Interphase, ( $\blacksquare$ ) CaO, ( $\bigcirc$ ) Ca<sub>7</sub>Bi<sub>10</sub>O<sub>22</sub>, ( $\blacktriangledown$ ) SrCO<sub>3</sub>.

spectra of chemical compounds in the system, which indicates that the same unknown phase may be formed in these samples, i.e. what we call interphase [5]. Now it has been determined that 2212 superconducting phase is formed through the interphase [5], which has yet to be indexed.

The Bi-Ca-O binary sample sintered at 730 °C mainly includes interphase and a small amount of  $Ca_7Bi_{10}O_{22}$ ; with rising sintering temperature, the former increases, the latter decreases. In Bi-Sr-Ca-O ternary samples, at the same sintering temperature, the amount of  $Ca_7Bi_{10}O_{22}$  is much smaller. For the samples sintered at 815 °C in both systems,  $Ca_7Bi_{10}O_{22}$  disappears, only interphase, a small amount of free CaO and the remaining SrCO<sub>3</sub> being present. Therefore, it is reasonable to think that Bi-Ca-O binary interphase is formed by the trans-



Figure 2 XRD patterns (low-angle part) of the BiCa<sub>y</sub>O<sub>1.50+y</sub> (y = 0.50, 0.75, 1.00, 1.25, 1.50, 1.75) samples sintered at 800 °C for 15 h. ( $\bullet$ ) Interphase, ( $\blacksquare$ ) Ca<sub>7</sub>Bi<sub>10</sub>O<sub>22</sub>, ( $\blacktriangle$ ) Ca<sub>7</sub>Bi<sub>6</sub>O<sub>16</sub>.

formation of  $Ca_7Bi_{10}O_{22}$ . The existence of strontium is favourable to the transformation to interphase containing strontium. Whether or not it is a binary or ternary system, mono-interphase can be obtained through the adjustment of compositions and sintering conditions.

The XRD patterns (low-angle part) of the samples with nominal composition  $BiCa_yO_{1,5+y}$  (y = (0.50-1.75) are shown in Fig. 2. For y = 0.50, the lower calcium sample, no interphase but many miscellaneous phases and some Ca<sub>7</sub>Bi<sub>10</sub>O<sub>22</sub> are formed. With the increasing y, interphase begins to emerge, the amount increasing accordingly and reaching its highest value for y = 1.00; but with the further increase in y, the amount of interphase decreases; if y > 1.25, it decreases dramatically and meantime Ca7Bi6O16 [8, 9] is formed. Only interphase is found in the y = 1.00 sample, while in the y = 1.25 sample, there is not only interphase but also some free CaO. Therefore, the ratio, y, of calcium to bismuth is important in the formation of binary mono-interphase, and the most suitable composition is y = 1.00. The microarea



Figure 3 XRD patterns of  $BiSr_xCa_{1-x}O_{2.50}$  with different strontium contents.

| TABLE I | I X-ray p | owder di | ffraction | data of | BiCaO <sub>2.50</sub> |  |
|---------|-----------|----------|-----------|---------|-----------------------|--|
|         |           |          |           |         |                       |  |

| hkl              | d <sub>obs</sub><br>(nm) | d <sub>cal</sub><br>(nm) | $I/I_0$ | hkl             | d <sub>obs</sub><br>(nm) | d <sub>cal</sub><br>(nm) | I/I <sub>0</sub> |
|------------------|--------------------------|--------------------------|---------|-----------------|--------------------------|--------------------------|------------------|
| 101              | 1.234                    | 1.240                    | 9       | 604             | 0.2543                   | 0.2546                   | 6                |
| 101              | 1.036                    | 1.041                    | 6       | 503             | 0.2479                   | 0.2481                   | 7                |
| 200              | 0.9000                   | 0.9035                   | 15      | 305             | 0.2437                   | 0.2439                   | 8                |
| 002/002          | 0.7202                   | 0.7218                   | 3       | 215             | 0.2357                   | 0.2353                   | 2                |
| $20\overline{2}$ | 0.6163                   | 0.6204                   | 2       | 800             | 0.2260                   | 0.2259                   | 2                |
| 30Ī              | 0.5941                   | 0.5948                   | 2       | 713             | 0.2244                   | 0.2240                   | 2                |
| 301              | 0.5227                   | 0.5237                   | 9       | 801             | 0.2175                   | 0.2173                   | 13               |
| 103              | 0.4860                   | 0.4870                   | 14      | $024/02\bar{4}$ | 0.2150                   | 0.2153                   | 4                |
| 400              | 0.4510                   | 0.4518                   | 52      | 705             | 0.2120                   | 0.2121                   | 18               |
| 103              | 0.4449                   | 0.4457                   | 5       | 415             | 0.2081                   | 0.2081                   | 16               |
| 303              | 0.4134                   | 0.4136                   | 6       | 007/007         | 0.2063                   | 0.2062                   | 10               |
| 112              | 0.4085                   | 0.4092                   | 3       | 516             | 0.2025                   | 0.2028                   | 5                |
| $31\overline{2}$ | 0.3690                   | 0.3694                   | 4       | 522             | 0.2008                   | 0.2007                   | 3                |
| 403              | 0.3635                   | 0.3632                   | 7       | 805             | 0.1959                   | 0.1956                   | 6                |
| 204              | 0.3583                   | 0.3578                   | 14      | 621             | 0.1953                   | 0.1953                   | 7                |
| 303              | 0.3468                   | 0.3470                   | 5       | 207             | 0.1933                   | 0.1937                   | 6                |
| 113              | 0.3423                   | 0.3429                   | 26      | 317             | 0.1928                   | 0.1929                   | 4                |
| 501              | 0.3358                   | 0.3367                   | 13      | 417             | 0.1886                   | 0.1888                   | 3                |
| 204              | 0.3170                   | 0.3163                   | 3       | 108             | 0.1827                   | 0.1826                   | 6                |
| 511              | 0.3035                   | 0.3025                   | 80      | 008/008         | 0.1805                   | 0.1804                   | 5                |
| 600              | 0.3007                   | 0.3012                   | 100     | 707             | 0.1772                   | 0.1772                   | 7                |
| 105              | 0.2929                   | 0.2933                   | 43      | 407             | 0.1763                   | 0.1761                   | 10               |
| 305              | 0.2801                   | 0.2805                   | 12      | 903             | 0.1748                   | 0.1746                   | 17               |
| 105              | 0.2771                   | 0.2775                   | 4       | 218             | 0.1732                   | 0.1735                   | 9                |
| 503              | 0.2668                   | 0.2670                   | 6       | 208             | 0.1714                   | 0.1712                   | 15               |
| 205              | 0.2616                   | 0.2618                   | 3       | 1013            | 0.1702                   | 0.1706                   | 8                |

composition analysis of the interphase by EDXS gives y = 1.07, so the composition of Bi–Ca–O binary interphase is very close to BiCaO<sub>2.50</sub>.

terns involve five groups of relatively concentrated characteristic peaks at about  $2\theta = 6^{\circ}-10^{\circ}$ ,  $16^{\circ}-20^{\circ}$ ,  $23^{\circ}-27^{\circ}$ ,  $41^{\circ}-44^{\circ}$  and  $51^{\circ}-53^{\circ}$ , respectively. With x varying between 0.00 and 0.67, almost all the peaks in the patterns correspond with one another, and when x

Fig. 3 shows the XRD patterns of  $BiSr_xCa_{1-x}O_{2.50}$  samples with different strontium contents. The pat-

TABLE III X-ray powder diffraction data of  $BiSr_{0.50}Ca_{0.50}O_{2.50}$ 

| hkl     | d <sub>obs</sub><br>(nm) | d <sub>cal</sub><br>(nm) | I/I <sub>0</sub> | hkl                  | d <sub>obs</sub><br>(nm) | d <sub>cal</sub><br>(nm) | I/I <sub>0</sub> |
|---------|--------------------------|--------------------------|------------------|----------------------|--------------------------|--------------------------|------------------|
| 101     | 1.264                    | 1.261                    | 7                | 205                  | 0.2961                   | 0.2958                   | 6                |
| 101     | 1.063                    | 1.062                    | 4                | 005/005              | 0.2946                   | 0.2945                   | 4                |
| 200     | 0.9210                   | 0.9188                   | 7                | 305                  | 0.2857                   | 0.2855                   | 8                |
| 002/002 | 0.7366                   | 0.7362                   | 2                | 503                  | 0.2727                   | 0.2723                   | 6                |
| 301     | 0.6062                   | 0.6041                   | 2                | 604                  | 0.2587                   | 0.2586                   | 5                |
| 301     | 0.5342                   | 0.5336                   | 5                | 505                  | 0.2525                   | 0.2522                   | 4                |
| 302     | 0.5175                   | 0.5172                   | 2                | 305                  | 0.2497                   | 0.2490                   | 5                |
| 103     | 0.4971                   | 0.4962                   | 13               | 215                  | 0.2390                   | 0.2390                   | 2                |
| 400     | 0.4602                   | 0.4594                   | 30               | 514                  | 0.2190                   | 0.2189                   | 14               |
| 112     | 0.4117                   | 0.4115                   | 2                | 705                  | 0.2156                   | 0.2155                   | 13               |
| 312     | 0.3723                   | 0.3716                   | 3                | 107                  | 0.2131                   | 0.2132                   | 10               |
| 403     | 0.3691                   | 0.3690                   | 8                | 415                  | 0.2117                   | 0.2115                   | 7                |
| 204     | 0.3648                   | 0.3643                   | 6                | 007/007              | 0.2102                   | 0.2103                   | 6                |
| 402     | 0.3625                   | 0.3624                   | 11               | 216                  | 0.2096                   | 0.2092                   | 5                |
| 303     | 0.3549                   | 0.3541                   | 4                | 207                  | 0.1978                   | 0.1977                   | 6                |
| 113     | 0.3466                   | 0.3463                   | 21               | 605                  | 0.1961                   | 0.1959                   | 4                |
| 501     | 0.3433                   | 0.3428                   | 10               | $008/00\overline{8}$ | 0.1842                   | 0.1841                   | 4                |
| 312     | 0.3382                   | 0.3373                   | 4                | 707                  | 0.1802                   | 0.1802                   | 4                |
| 204     | 0.3237                   | 0.3228                   | 6                | 903                  | 0.1778                   | 0.1778                   | 13               |
| 600     | 0.3072                   | 0.3063                   | 100              | 218                  | 0.1767                   | 0.1764                   | 7                |
| 511     | 0.3055                   | 0.3053                   | 62               | 208                  | 0.1747                   | 0.1747                   | 12               |
| 105     | 0.2993                   | 0.2990                   | 34               | 1013                 | 0.1730                   | 0.1730                   | 6                |

TABLE IV Lattice parameters of  $BiSr_xCa_{1-x}O_{2.50}$ 

| $BiSr_xCa_{1-x}O_{2.50}$                                  | <i>a</i> (nm) | <i>b</i> (nm) | c (nm) | β (deg) | V (nm <sup>3</sup> ) |
|---|---------------|---------------|--------|---------|----------------------|
| BiCaO <sub>2,50</sub>                                     | 1.8363        | 0.5366        | 1.4670 | 100.26  | 1.42241              |
| $BiSr_{0.25}Ca_{0.75}O_{2.50}$                            | 1.8563        | 0.5356        | 1.4820 | 99.95   | 1.45129              |
| BiSr <sub>0.33</sub> Ca <sub>0.67</sub> O <sub>2.50</sub> | 1.8588        | 0.5345        | 1.4869 | 99.96   | 1.45501              |
| $BiSr_{0.50}Ca_{0.50}O_{2.50}$                            | 1.8661        | 0.5341        | 1.4952 | 100.03  | 1.46747              |
| BiSr <sub>0.67</sub> Ca <sub>0.33</sub> O <sub>2.50</sub> | 1.8676        | 0.5330        | 1.4983 | 100.04  | 1.46861              |
| BiSr <sub>0.75</sub> Ca <sub>0.25</sub> O <sub>2.50</sub> | 1.8761        | 0.5331        | 1.5014 | 100.08  | 1.47845              |



Figure 4 Indexed XRD pattern of BiCaO<sub>2.50</sub>.



Figure 5 Indexed XRD pattern of BiSr<sub>0.50</sub>Ca<sub>0.50</sub>O<sub>2.50</sub>.

= 0.75, the five groups of characteristic peaks still exist but some apparently new peaks appear. All diffraction peaks for every sample can be indexed as interphase (see below), that is, the samples only involve interphase. Meanwhile, all 20 values shift towards low-angle with increasing x. Thus, the interphase is a solid solution of Bi-Ca-O and Bi-Sr-O; its composition should be BiSr<sub>x</sub>Ca<sub>1-x</sub>O<sub>2.50</sub>. With x increasing up to 0.75, the structural frame of BiSr<sub>x</sub>Ca<sub>1-x</sub>O<sub>2.50</sub> remains unchanged.

# 3.2. The solid solution structure of BiSr<sub>x</sub>Ca<sub>1-x</sub>O<sub>2.50</sub>

Previously [6], we have preliminarily indexed the BiCaO<sub>2.50</sub> binary interphase. However, our present work on the solid-solution structure of BiSr<sub>x</sub>Ca<sub>1-x</sub>O<sub>2.50</sub> has found that the previous crystallography data of BiCaO<sub>2.50</sub> cannot be applied to BiSr<sub>x</sub>Ca<sub>1-x</sub>O<sub>2.50</sub> when  $x \neq 0$ . BiSr<sub>x</sub>Ca<sub>1-x</sub>O<sub>2.50</sub> is strontium and calcium solid solution. The structures of BiSr<sub>x</sub>Ca<sub>1-x</sub>O<sub>2.50</sub> should maintain consistency. Thus the previous data of BiCaO<sub>2.50</sub> should be revised. The structures of BiSr<sub>x</sub>Ca<sub>1-x</sub>O<sub>2.50</sub> is now discussed in detail.

The diffraction lines of  $BiSr_xCa_{1-x}O_{2.50}$  were indexed using Werner's TREOR program [7] and the indexed powder diffraction data are listed in Tables II and III, and the X-ray powder diffraction patterns are illustrated in Figs 4 and 5. The crystals of  $BiSr_xCa_{1-x}O_{2.50}$  have a monoclinic unit cell with space group P1m1 or P12/m1 and the unit cell parameters are listed in Table IV.

The calculated interplanar distances,  $d_{cal}$ , agree well with the observed ones,  $d_{obs}$ , when x varies between 0.00 and 0.67 (see Tables I and II). But when x = 0.75, the deviations between  $d_{cal}$  and  $d_{obs}$  for some peaks are somewhat large. The reason for this is that excessive strontium solid solubility makes its crystal structure distort greatly and its diffraction peaks broaden, which makes it difficult to obtain accurate  $2\theta$  values. Fig. 6 shows the variation of a, b, c and the volume, V, of the unit cell with strontium solid solubility, x. The a, b, c and V vary linearly with the increasing strontium solid solubility, x, from 0.00 up to 0.33, and gradually tend to saturate at about x = 0.50. But the *a* and *V* increase suddenly at about x = 0.67. Therefore, we can infer that the strontium solid solubility limit of BiSr,- $Ca_{1-x}O_{2.50}$  is between 0.67 and 0.75, and beyond this limit the crystal structure is greatly distorted.



Figure 6 Lattice parameters ( $\blacksquare$ ) a, ( $\blacktriangledown$ ) b, ( $\blacktriangle$ ) c and ( $\bigcirc$ ) V of BiSr<sub>x</sub>Ca<sub>1-x</sub>O<sub>2.50</sub> dependence of strontium solid solubility x = Sr/Sr + Ca.



Figure 7 Scanning electron micrographs of interphase with different strontium solid solubilities. (a) x = 0.50, (b) x = 0.75.

Scanning electron micrographs of the interphase with different strontium solid solubility are shown in Fig. 7 and reveal that plate-like morphology for lower strontium interphase (x = 0.50) becomes a powdery morphology for high strontium interphase (x = 0.75), which apparently results from the structure distortion of the interphase containing excessive strontium.

### 4. Conclusion

BiSr<sub>x</sub>Ca<sub>1-x</sub>O<sub>2.50</sub> is the solid solution of Bi–Ca–O and Bi–Sr–O. The strontium dissolved in the phase reaches saturation when its solid solubility x = Sr/Sr + Ca = 0.50, while the strontium solid solubility limit of the phase is between 0.67 and 0.75. The crystallographic data of BiSr<sub>x</sub>Ca<sub>1-x</sub>O<sub>2.50</sub> are also given.

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